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**Finite Element Optimization for Nondestructive Evaluation
on a Graphics Processing Unit for Ground Vehicle Hull
Inspection**

Paper presented at 2013 NDIA/GVSETS Conference, Aug 22 2013

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Finite Element Optimization for Nondestructive Evaluation on a Graphics Processing Unit for Ground Vehicle Hull Inspection

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**FINITE ELEMENT OPTIMIZATION FOR NONDESTRUCTIVE
EVALUATION ON A GRAPHICS PROCESSING UNIT FOR GROUND
VEHICLE HULL INSPECTION**

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ABSTRACT

Shape reconstruction for nondestructive evaluation (NDE) of internal defects in ground vehicle hulls using eddy current probes provides a rationale for determination of when to withdraw vehicles from deployment. This process requires detailed finite element optimization and is computationally intensive. Traditional shared memory parallel systems, however, are prohibitively expensive and have limited central processing units (CPUs), making speedup limited. So parallelization has never been done. However, a CPU that is connected to graphics processing units (GPUs) with effective built-in shared memory provides a new opportunity. We implement the naturally parallel, genetic algorithm (GA) for synthesizing defect shapes on GPUs. Shapes are optimized to match exterior measurements, launching the parallel, executable GA kernel on hundreds of CUDA™ (Compute Unified Device Architecture) threads to establish the efficiencies.

MOTIVATION AND BACKGROUND

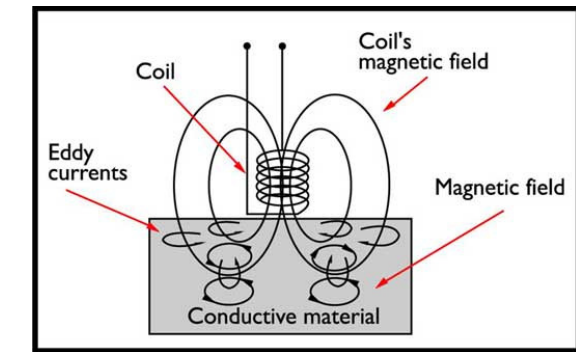
When a hull or plate-plate weld in a ground vehicle is found to be defective, it is often wastefully taken out of service for repairs in present practice without determining if the defect warrants withdrawal. A procedure is required for defect characterization so that a decision to withdraw may be thought-out without compromise to war-fighter-safety; such a procedure would include behind-armor damage created by Improvised Explosive Device (IED) blasts. X-ray technology is not only dangerous, but also impracticable because of requiring readings within the tank's interior of X-rays that pass through the hull. NDE for corrosion, cracks, and other defects in ground vehicle armor employs eddy current probes for testing [1]. Recent changes have been

towards composite materials for ground vehicles and remote measurement of defects through sophisticated measuring devices. These methods do not deal with corrosion and ignore the larger fleets of steel-hulled ground vehicles continuing to require the older NDE assessment. These conventional vehicles with steel hulls will remain in service for extended periods and be increasingly aging so that testing for, and characterizing defects are *a fortiori* important

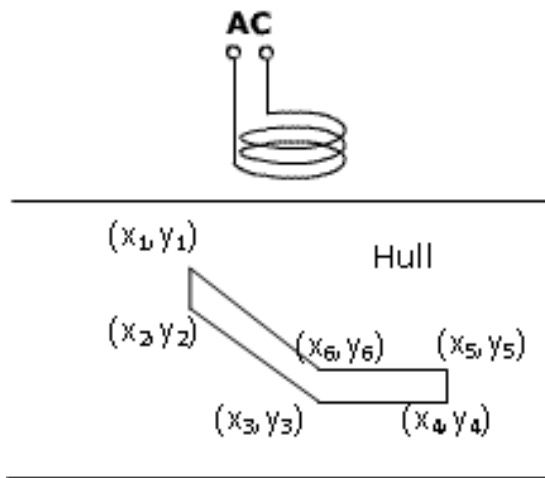
STATE OF THE ART – HOW IT IS DONE TODAY

Present methodology examines the response of the hull under test to a signal from an eddy current problem [1] (Fig. 1a). Any deviation from a known baseline response of a

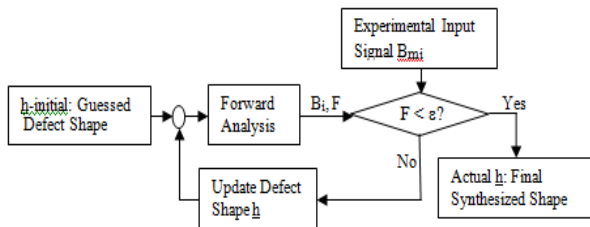
target with no defects is flagged as defective. Defect characterization is not done at present because it involves thousands of tedious eddy current computations in complex arithmetic and a three-dimensional magnetic vector potential with mixed finite elements [2] to model and optimize the defect shape \underline{h} of Fig. 1b until the computed and measured fields match (Fig. 1c).



(a) The Test System

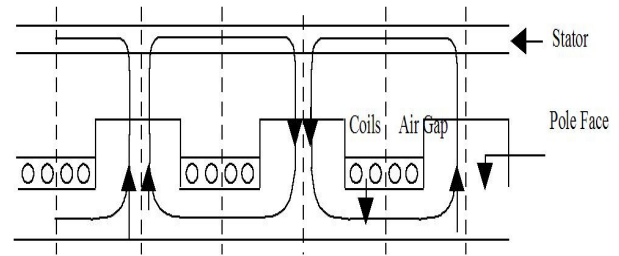


(b) Defect Modeled as $\underline{h} = \{x_1, y_1, \dots, y_6\}$

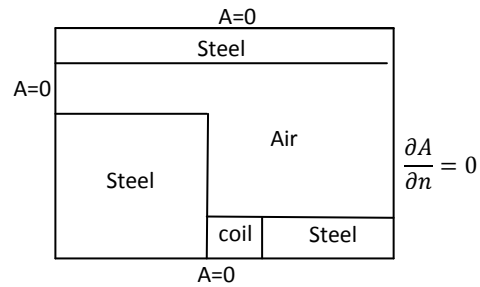


(c) Reconstructing \underline{h}

Figure 1: Eddy Current Defect Testing System



a) Physical Alternating Pole System



b) Minimum Boundary Value Problem with Boundary Conditions on Magnetic Vector Potential A

Figure 2: Pole-Faces to be Shaped and Problem

THE TEST PROBLEM

Gradients-based optimization is difficult to program especially with eddy currents and would require a costly shared memory system usually limited to 16 processors because of technology limits [3]. Time is also a factor because these computations require large computer systems not readily portable for field testing. MSU's HPCC (High

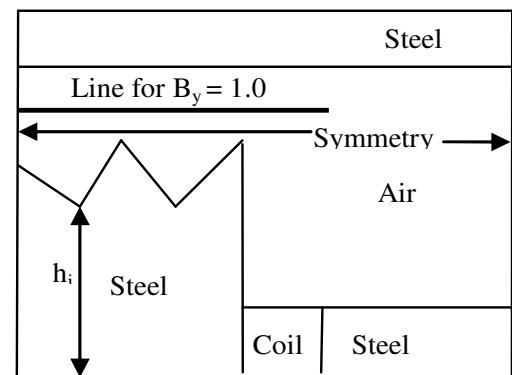


Figure 3: Parametric Model of Pole Face with Measuring Points

Performance Computing Center) Cluster provides an alternative powerful platform with parallel processing on the Graphics Processing Unit (GPU) [4, 5].

A primary question occupying our minds was which optimization method to use.

Our experience is that gradient techniques are fast in computation but slow to set up because of the programming time to have special mesh generators. Going by the literature, Preis *et al.* [6], staunch advocates of the zeroth order evolution strategy, merely say it is competitive with its higher order deterministic counterparts (which we take to mean the equivalent in time at best), but claim that its “robustness and generality” are superior. We agree with this observation because search methods will never see local minima as a problem. In contrast to what Preis *et al.* state, Simkin and Trowbridge [7] observe that simulated annealing and the evolution strategy take many more function evaluations. This is also our experience and we would add that the genetic algorithm works faster than simulated annealing. Haupt [8] advises that the genetic algorithm is best for many discrete parameters and the gradient methods for where there are but a few continuous parameters. However, we have gone up to 30 continuous parameters without problems. There seemed good reasons to go either way. But when the need for special mesh generators for high order methods is considered, a zeroth order method [9] is best.

For now therefore in this feasibility study, a zeroth order method like the genetic algorithm or simulated annealing has been selected to be the best choice. These involve two zeroth order methods where no derivative calculations are required. They avoid the difficult computation of objective function gradients and the need for special mesh generators [9]. The simple test problem of Fig. 2 was selected. Fig. 2a shows the alternating poles pushing flux up and down in adjacent sets and Fig. 2b the minimal boundary value for the magnetic vector potential A with governing equation:

$$-\frac{1}{\mu} \nabla^2 A = J \quad (1)$$

where μ is the magnetic permeability and J is the forcing current density in the coils [2].

Table 1: Hitting the 4 GB Limit at Matrix Size $10^4 \times 10^4$

| Size | TE | SK(in MB) | TENSIP | SK(in MB) | TENSIS | SC(MB) |
|-------|-----------|------------|---------|-----------|--------|----------|
| 100 | 10000 | 0.038147 | 661 | 0.002521 | 1209 | 0.004612 |
| 400 | 16000 | 0.061035 | 8819 | 0.033642 | 2421 | 0.009235 |
| 900 | 810000 | 3.089905 | 28829 | 0.109974 | 5021 | 0.019153 |
| 1600 | 2560000 | 9.765625 | 67239 | 0.256496 | 10421 | 0.039753 |
| 2500 | 6250000 | 23.841858 | 130049 | 0.496098 | 17301 | 0.065998 |
| 6000 | 36000000 | 137.329101 | 374459 | 1.428448 | 41681 | 0.159000 |
| 8000 | 64000000 | 244.140625 | 657679 | 2.508846 | 54221 | 0.206836 |
| 10000 | 100000000 | 381.469727 | 1020099 | 3.891369 | 68021 | 0.259479 |

Key:

TE: Total Elements

TENSIP: Total number of elements that need to be stored in profile storage

TENSIS: Total number of elements that need to be stored in sparse storage

SK: Storage capacity

The object is to optimize the shape of the pole-face with GA. Thus as shown in Fig. 3, where the pole face is defined by 5 heights h_1, h_2, \dots, h_5 . These five heights h_i of Fig. 3 had to be optimized to get the pole shape giving us a vertical flux density 1 T along a line above the pole face. To define this formally the m measuring points were defined along the line show in Fig. 3. We allowed m to be changeable but used 3 which worked well. This performance requirement of 1 T was imposed through the least-square objective function

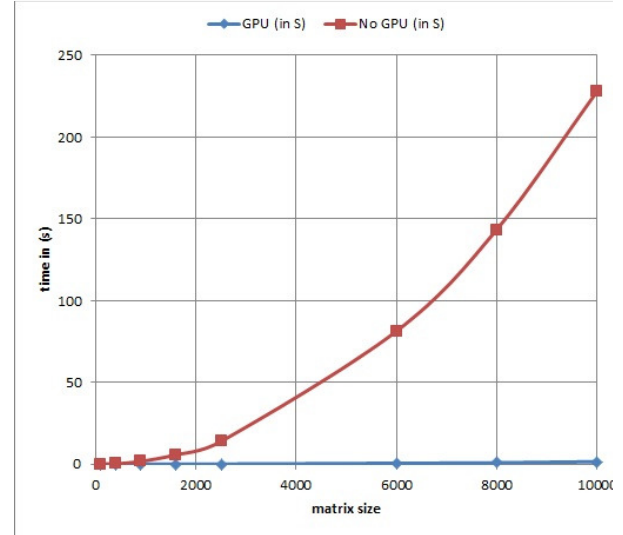


Figure 4: Timing by Element-by-Element Iterations (with GPU is the flat horizontal line)

$$F = \sum_{i=1}^m (B_{Computed}^{y,i} - 1.0)^2 \quad (2)$$

where B^y is the vertical flux density. Thus as $B_{Computed}^{y,i} \rightarrow 1$, F would tend to zero. The heights h , clearly would determine the value of F making

$$F = F(h_1, h_2, \dots, h_5) \quad (3)$$

Thus an optimization method [10-12] needs to be pressed into service to determine these values of h_1, h_2, \dots, h_5 that would make F zero.

GPU PROCESSING – RESULTS

From the time Marrocco and Pironneau [10], and Gitosusastro, Coulomb and Sobonnadiere [11] applied gradients based finite elements to optimize magnetic circuits, papers have appeared using various optimization techniques [12]. Searching for the minimum requires several evaluations of the objective function F for each set h_1, h_2, \dots, h_5 being tested. This means a new mesh and a large computational load. Shared memory parallel computers have been used [13, 14] but these are expensive, costly and the technology limits the number of processors that can be

used, usually to 16. However, since recently parallelization has been possible on a commonly available PC itself with 4 cores, where the code may simultaneously run on the multiple cores or the graphics processing unit (or GPU – to be more specific on an NVIDIA GPU with CUDA architecture [4]). There is however a severe memory limit – 4 GB at present. This would limit large problems as well as optimization where several problems may be attempted at once. We tested how the 4 GB translates into matrix size and the results of this study are shown in Table 1. It is seen that the limit is a 10,000x10,000 matrix size when the most efficient (sparse) storage scheme is employed [2].

For our purposes, as the project progresses, we need to solve eddy current problems in three dimensions. That is, if we are dealing with the magnetic vector potential as the state variable, it would have three components with each component a complex number. The implications to matrix storage would be severely limiting.

To overcome this we propose to use a method of the early 1980s when, working with the then new IBM PC 286, we had a memory limit of 612 kB which could not hold even a trivial matrix in memory. What we used to do was employ the Jacobi methods of matrix solution element-by-element. For example in solving the finite element matrix equation

$$[P]\{A\} = \{Q\} \quad (4)$$

just to explain the issues, the Gauss-Seidel iterative method [2], commonly used by power engineers, is an improvement on the older Gauss iterations where in each iteration m+1 we use the latest available values of the unknowns A, using equation i of (4) to compute A_i treating only A_i as the unknown and all the other variables as known and given by their latest values:

$$A_i^{m+1} = \frac{1}{P_{ii}} \left\{ \sum_{k=1}^{i-1} P_{ik} A_k^{m+1} + \sum_{k=i+1}^n P_{ik} A_k^m \right\} \quad (5)$$

with obvious modifications for $i=1$ and $i=n$. Here at iteration m+1, computing A_i in the order $i=1$ to n , A is at values of iteration m+1 up to the (i-1)th component of {A} and at the values of the previous iteration m for values after i. The Gauss iterations using the old iteration's value for computing all A_i in iteration m+1 according to

$$A_i^{m+1} = \frac{1}{P_{ii}} \left\{ Q_i - \sum_{k=1}^{i-1} P_{ik} A_k^m - \sum_{k=i+1}^n P_{ik} A_k^m \right\} \quad (6)$$

is inefficient in the context of sequential computations. But in this case of parallelization, if we can resort to this conventionally inefficient method, we may not form the matrix [P]. If [D] is the matrix [P] with all off diagonal elements eliminated, then Gauss's iterative method in this modified form gives,

$$[D]\{A\}^{m+1} = \{Q\} - [P - D]\{A\}^m \quad (7)$$

Thus without forming [P], the operation of the right hand side of (7) can be effected by taking each finite element in

turn, computing the local 3x3 Dirichlet matrix $[P]^L$ and using that because

$$[P] = \sum_{Elements} [P]^L \quad (8)$$

So as each $[P]^L$ is formed, the three values of $\{A\}^m$ may be taken and subtracted as in the right hand side of (7). We tested this and the results are shown in Fig. 4. We were able to go up to matrix sizes 100,000x100,000 and well beyond. We then applied the same idea to the more efficient incomplete Cholesky preconditioned conjugate gradients (ICCG) method [2] as laid out by Mahinthakumar and Hoole [15] for shared memory systems. In the GA kernel, there was no internal parallelization. In this work, the Incomplete Cholesky Conjugate Gradients matrix solver was parallelized on the GPU and we observed a speed-up of 146.351 for the matrix size 10,000x10,000 (Fig. 5).

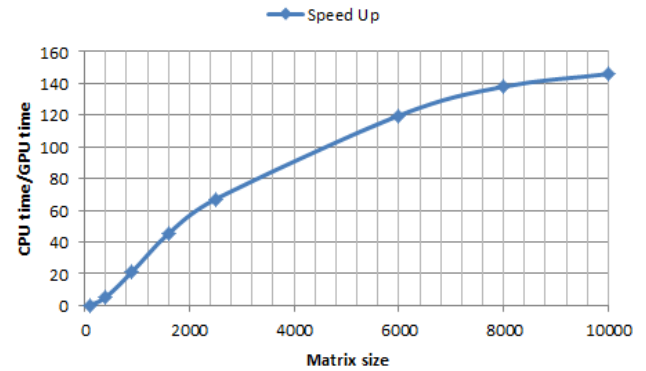


Figure 5: Conjugate Gradients Algorithm: Matrix Size Vs CPU time/GPU time

Table 2: Performance of GA

| Pop. Size | Error (%) | Fitness F | Obj. Function | Time (s) |
|-----------|-----------|-----------------------|---------------|----------|
| 10 | 6.7 | 0.94×10^{-4} | 1067.0 | 2.00 |
| 20 | 5.46 | 0.0018 | 554.55 | 3.88 |
| 50 | 2.09 | 0.9974 | 0.002 | 9.65 |

Table 3: Performance of SA

| Iterations | Object Funct F | Time (s) |
|------------|----------------|----------|
| 500 | 0.0448 | 14.25 |
| 1000 | 0.0146 | 28.22 |
| 4000 | 0.0282 | 119.12 |
| 40000 | 0.0075 | 1144.42 |

APPLICATION TO POLE FACE SHAPING

The pole face then shaped by optimization is shown in Fig. 6. GA was found to be effective converging faster than simulated annealing. The “fitness of the solution” for the GA, $1/(1+F)$, would approach 1 from below. The population size is the number of GA kernels launched as GPU threads. The optimal shape is in Fig. 5 and details in Tables 2 and 3 where the performances of the genetic algorithm and simulated annealing are respectively summarized. After 50 threads, the fitness was excellent. To compare the timings, for the genetic algorithm, a comparable object function is computed in Table 2 from the fitness F : $(1 - F)/F$. It is seen that the genetic algorithm reaches a comparable object function value much faster than simulated annealing.

Seeking large population sizes and matrix size, we attempted to estimate the gain by using the GPU. The results are shown in Table 4. We observed these results for a simple electro-thermal coupled problem with the matrix size 204×204 .

TEST PROBLEM OF INVERSION

To test our methodology and establish feasibility for these methods mooted, we need a special mesh generator modeling the crack defined by parametric location and shape. We created such a mesh generator just for the crack assessment problem, created a crack and computed the fields along measuring points outside the steel plate.

Thereafter, taking the results as the “measured field,” we had to discover this crack as described by parameters $\{p\}$.

The results are shown in Fig. 7. We obtained a 95% match. In realistic cracks however, no model would be perfectly valid so the objective function will not go down to zero. However, the method is seen to be feasible.

CONCLUSIONS

We conclude that using genetic algorithm optimization doing computations on a GPU for the reconstruction of hull defects has enormous benefits – speed through parallelism and convenience in avoiding computationally expensive gradients which are almost impossible to program as general purpose software.

Ultimately this problem would need to be done in 3-D

Table 4: Gain in using GPU

| Population Size | No of Iterations | Time(s) | | Ratio GPU/CPU Times |
|-----------------|------------------|----------|---------|---------------------|
| | | CPU | GPU | |
| 50 | 20 | 4824.94 | 432.38 | 11.16 |
| 100 | 20 | 9619.24 | 475.09 | 20.25 |
| 200 | 20 | 18322.20 | 667.85 | 27.43 |
| 400 | 20 | 37444.20 | 1480.32 | 25.29 |
| 512 | 20 | 49200.00 | 1756.43 | 28.01 |

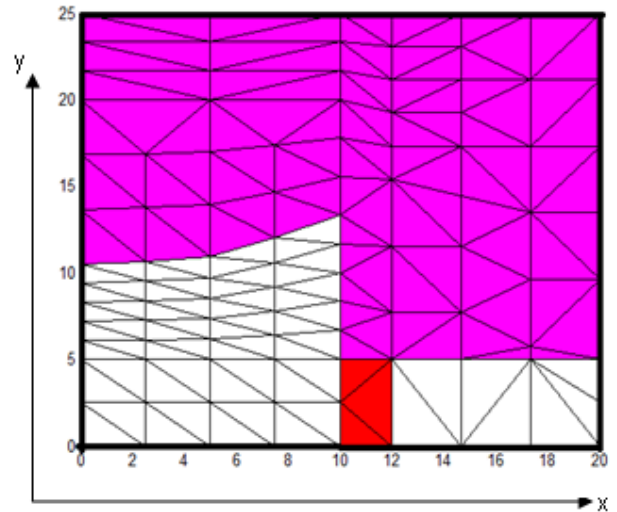


Figure 6: An Optimized Pole-face (5 parameters, 98 nodes, and 70 unknowns)

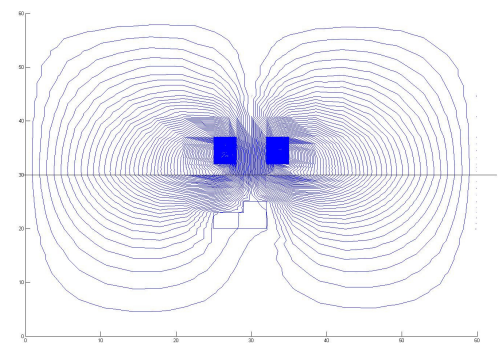


Figure 7: Crack Recreated from Exterior Fields using 10 parameters

where the computational load would be higher. Special mesh generators that maintain nodal connections would add to the burden. Additionally, many parameters must be allowed to get accurate crack shapes.

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